

ANALYSIS OF OPTICALLY CONTROLLED MICROWAVE/MILLIMETER WAVE DEVICE STRUCTURES

Raine N. Simons* and Kul B. Bhasin

National Aeronautics and Space Administration
 Lewis Research Center
 Cleveland, Ohio

ABSTRACT

The light-induced voltage and the change in the source-to-drain channel current under optical illumination higher than the semiconductor bandgap for GaAs MESFET, InP MESFET, $Al_{0.3}Ga_{0.7}As/GaAs$ high electron mobility transistor (HEMT) and GaAs permeable base transistor (PBT) were analytically obtained. The GaAs PBT and GaAs MESFET have much higher sensitivity than InP MESFET. The $Al_{0.3}Ga_{0.7}As/GaAs$ HEMT is observed to have the highest sensitivity. Variation in device parasitics due to optical illumination and its effect on the cutoff frequencies f_T and f_{max} are also investigated.

INTRODUCTION

Direct optical control of microwave devices in GaAs monolithic microwave integrated circuits (MMIC's) can result in better switching, amplitude and phase control in amplifiers, and frequency control in oscillators (1). Furthermore, it allows use of optical fiber technology for the inter-connecting MMIC's, thereby reducing cross talk and electromagnetic interference. It also enhances efficiency and speed of operation (2).

Several authors have experimentally investigated the effect of light on the dc characteristics of GaAs metal semiconductor field effect transistor (MESFET) (3,4) and its effect on the S-parameters (5). The optical absorption coefficient and energy bandgap of III-V compound semiconductors can be tailored to a particular wavelength by adjusting the mole fraction (x) of its constituents (6). Besides, the III-V compound semiconductor devices can be integrated with other MMIC components on a single semi-insulating GaAs or InP substrate (7). These offer further advantages for direct optical control of microwave devices.

We investigated the effect of light on several III-V compound semiconductor devices, such as, GaAs MESFET, InP MESFET, $Al_xGa_{1-x}As/GaAs$ high electron mobility transistor (HEMT), and GaAs Permeable Base Transistor (PBT). The computed results illustrate (a) the light-induced voltage as a function of the incident optical power density, (b) the change in the drain current, with change in optical power density, as a function of the drain to source voltage, and (c) the variation in the device

parasitics due to optical illumination and its effect on the cutoff frequencies f_T and f_{max} .

LIGHT INDUCED VOLTAGE

The operation of these microwave devices as photodetectors and amplifiers depend on the photo-generation of electron-hole pairs in their active layer. Figure 1 illustrates several techniques for the direct optical control of microwave solid-state devices. In these techniques light from a laser or a light-emitting diode (LED)(14) or an optical waveguide (15) is made to strike the active layer of the device. The incident optical power increases the concentration of the minority carriers, for example, the holes in an n-type channel. This increase in hole concentration Δp is proportional to the incident optical power P_{opt} , the wavelength of the incident light λ , the optical absorption coefficient of the semiconductor α , the thickness of the active layer d , and the minority carrier life time τ . Expressed mathematically, Δp is (8,9)

$$\Delta p = \frac{\tau}{d} \left[\frac{P_{opt} \lambda}{hc} \right] \left(1 - e^{-\alpha d} \right) \quad (1)$$

where h is Planck's constant (6.62617×10^{-34} J sec) and c is the speed of light in vacuum (2.99792×10^8 m/sec). The quantity inside the square brackets represents the number of photons of wavelength λ falling on unit area per second.

The light-induced voltage V_{lit} is expressed as (8,9)

$$V_{lit} = \frac{KT}{q} \ln \left(\frac{p + \Delta p}{p} \right) \quad (2)$$

where K is Boltzmann's constant (1.38066×10^{-23} J/K), T is the absolute temperature, q is the electronic charge (1.60218×10^{-19} C), and p is the equilibrium minority carrier concentration in the active layer (e.g., holes in an n-type channel) and is given by (8)

$$p = \frac{n_i^2}{n} \quad (3)$$

where n_i is the intrinsic carrier concentration ($1.79 \times 10^{16}/cm^3$) and n is the carrier concentration.

*NRC-NASA Research Associate.

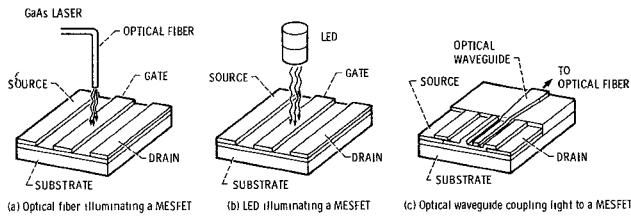


Fig 1 - Proposed techniques for direct optical control of microwave devices

EFFECT OF LIGHT ON DRAIN CHARACTERISTICS

The drain current I_d as a function of the applied gate bias voltage V_{gs} and the drain to source voltage V_{ds} for a MESFET is expressed as (8,9)

$$I_d = \frac{qmnwd}{P} \left\{ V_{ds} - \frac{2}{3} \frac{1}{V_p^{1/2}} \right. \\ \left. \times \left[(V_{ds} + V_b - V_{gs})^{3/2} - (V_b - V_{gs})^{3/2} \right] \right\} \quad (4)$$

where μ is the electron mobility ($5300 \text{ cm}^2 \text{ V sec}$), W and L are the gate width and length, respectively, V_b is the built-in Schottky barrier voltage, and V_p is the pinch-off voltage required to completely deplete the active layer, such that

$$V_p = \frac{qnd^2}{2\epsilon_0\epsilon_r} \quad (5)$$

In Eq. (5) ϵ_0 is the permittivity in vacuum ($8.85418 \times 10^{-12} \text{ F/mt}$), and ϵ_r is the relative permittivity of the active layer. Illuminating the MESFET is equivalent to forward biasing the gate of the MESFET by a voltage source equal to V_{lit} . The net voltage at the gate is therefore a superposition of the gate bias V_{gs} and V_{lit} .

The drain current I_{ds} for a depletion-mode (normally ON) HEMT is expressed as (10)

$$I_d = (37.8V_{gs} - 158V_{gs}^2 - 360V_{gs}^3 + 18.5) \\ \times \tan^{-1} \left(\frac{V_{ds}}{0.07 + 0.1V_{gs}} + 0.25V_{ds} \right) \quad (6)$$

For an enhancement-mode (normally off) HEMT, it is expressed as (10)

$$I_d = (49.8V_{gs} - 13.64) \tan^{-1} \left(\frac{V_{ds}}{0.143V_{gs}} + 0.5V_{ds} \right) \quad (7)$$

The net voltage at the gate is a superposition of V_{gs} and V_{lit} .

COMPUTED RESULTS

The thickness of the active layer, the gate width and length, and the doping density are presented in Fig. 2 for GaAs MESFET, InP MESFET, $\text{Al}_{0.3}\text{Ga}_{0.7}\text{As}/\text{GaAs}$ HEMT, and GaAs PBT. The properties of the semiconductors used in the fabrication of these microwave devices is presented

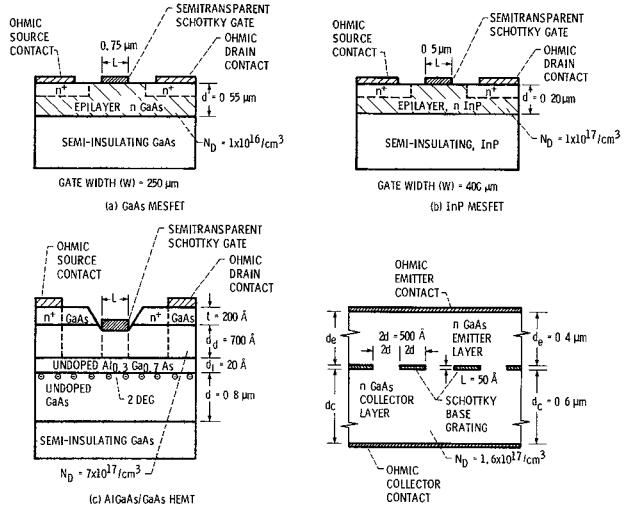


Fig. 2 - Material parameters of microwave device structures for direct optical control of monolithic microwave and millimeter-wave integrated circuits

in Table I. The computed light-induced voltage using Eq. (2) is presented in Fig. 3 as a function of the incident optical power density for the devices shown in Fig. 2. The light-induced voltage increases linearly with the incident optical power. Besides, at a fixed incident optical power density the $\text{Al}_{0.3}\text{Ga}_{0.7}\text{As}/\text{GaAs}$ HEMT had the highest sensitivity, and the InP MESFET the lowest sensitivity. The sensitivity of GaAs PBT and GaAs MESFET were almost identical and fall midway between those of HEMT and InP MESFET.

The drain current for a GaAs MESFET computed using Eq. (4) is illustrated in Fig. 4 for several optical power density and gate-to-source dc bias. In these computations the gate metallization was

TABLE I. - PROPERTIES OF SEMICONDUCTORS USED IN THE FABRICATION OF MICROWAVE DEVICES AT 300 K

Material	Electron mobility μ , $\text{cm}^2/\text{V sec}$	Intrinsic carrier concentration n_i , cm^{-3}	Optical absorption coefficient α , cm^{-1}	Wave length λ , μm	Minority carrier lifetime τ , sec	Relative permittivity, ϵ_r	Schottky barrier voltage, V_b
GaAs	5300	1.78×10^6	1.00×10^4	0.87	1×10^{-8}	13.1	Gold: 0.9 ITO: 0.95
InP	3300	1.97×10^9	1.80×10^4	1.06	1×10^{-8}	12.55	Gold: 0.5
$\text{Al}_{0.3}\text{Ga}_{0.7}\text{As}$	9000	2.5×10^3	1.25×10^4	0.653	2×10^{-8}	12.2	Gold: 1.11

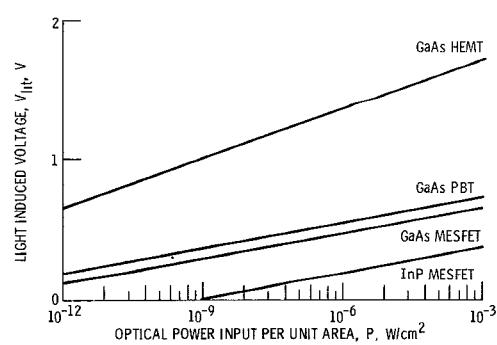


Fig. 3 - Light-induced voltage versus the incident optical power.

assumed to be gold, which is perfectly transparent to light. In practice, however, this is not true. This limitation can be overcome if the gate metalization is indium tin oxide. Indium tin oxide (ITO) is transparent to visible light (11) and forms a good Schottky contact with GaAs (12). The computed drain characteristics for a GaAs MESFET with an indium tin oxide gate is shown in Fig. 5. In Fig. 6 the ratio of the saturation drain current with and without illumination as a function of the gate-to-source voltage at a fixed incident optical power density for a GaAs MESFET is shown. This figure shows that the optical gain of a normally off FET is maximum if the gate-to-source bias is such that the FET is in pinch-off condition.

The drain current characteristics for a InP MESFET with a Au/(n) InP Schottky gate computed using Eq. (4) is shown in Fig. 7.

The drain current characteristics for depletion- and enhancement-mode $\text{Al}_{0.3}\text{Ga}_{0.7}\text{As}/\text{GaAs}$ HEMT's computed using Eqs. (6) and (7) are shown in Figs. 8 and 9, respectively.

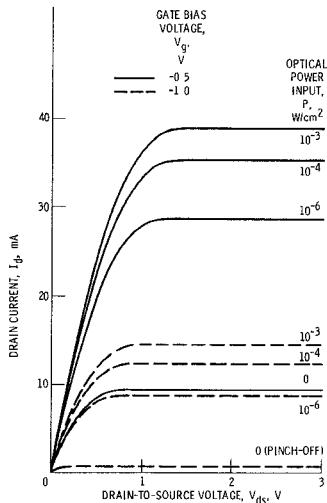


Fig. 4. - Drain current versus the drain-to-source voltage for GaAs MESFET with Au/(n) GaAs Schottky gate. Illumination wavelength, 0.87 μm

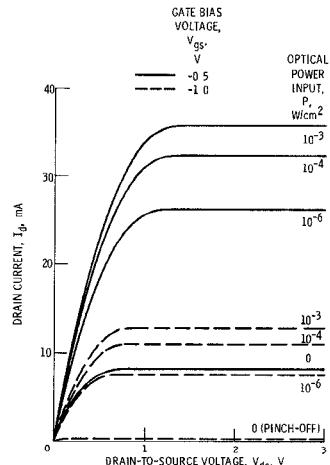


Fig. 5. - Drain current versus the drain-to-source voltage for GaAs MESFET with ITO/(n) GaAs Schottky gate. Illumination wavelength, 0.87 μm .

The change in the gate to source capacitance C_{gs} , with and without illumination, as a function of the gate-to-source bias for a GaAs MESFET (HFET-1000-01) is presented in Ref. (13). There, C_{gs} is observed to increase with illumination by as much as 30 percent. The increase in C_{gs} tends to lower the unity current gain frequency f_T and the unity maximum available gain frequency f_{max} . However, this change in C_{gs} is exploited in optically tuning FET oscillators.

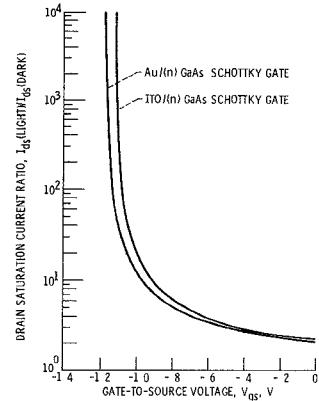


Fig. 6. - Ratio of drain saturation current with and without illumination versus the gate voltage for a GaAs MESFET with different Schottky gate configurations. The incident optical power level is kept constant

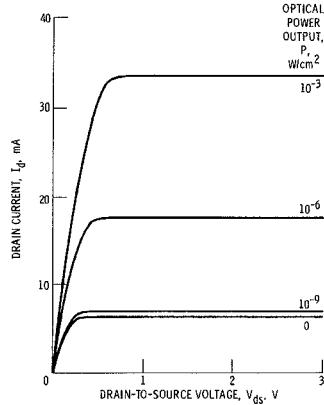


Fig. 7. - Drain current versus the drain-to-source voltage for InP MESFET with Au/(n) InP Schottky gate. Illumination wavelength, 1.06 μm , gate bias voltage, V_{gs} , -2 V

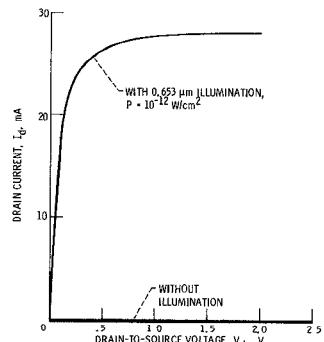


Fig. 8. - Drain current versus the drain-to-source voltage of a depletion-mode (normally on) AlGaAs/GaAs HEMT. Gate bias voltage, V_{gs} , -0.65 V

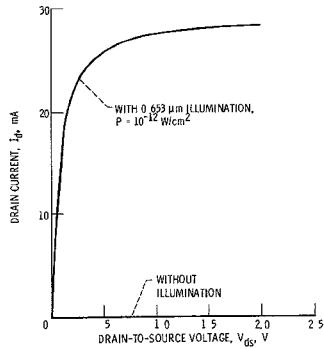


Fig. 9 - Drain current versus the drain-to-source voltage of an enhancement-mode (normally off) Al_{0.3}Ga_{0.7}As HEMT. Gate bias voltage, $V_{GS} = 0$

CONCLUSIONS

Light-induced voltages as a function of the incident optical power density for GaAs MESFET, InP MESFET, Al_{0.3}Ga_{0.7}As/GaAs HEMT and GaAs PBT were obtained. The drain current characteristics for these devices for various incident optical power densities were also obtained. The effect of light on the parasitics was qualitatively estimated.

The GaAs MESFET and PBT have much higher sensitivity to light than InP MESFET. However, the Al_{0.3}Ga_{0.7}As/GaAs HEMT has the highest sensitivity. The change in the drain current with illumination was significant. The increase in C_{GS} with illumination tended to lower f_T and f_{max} .

REFERENCES

1. R.G. Hunsperger, "Optical Control of Microwave Devices," Integrated Optical Circuit Engineering II, SPIE vol. 578, S. Sriram, ed., Bellingham: SPIE, pp. 40-45:Sept. 1985.
2. J. Austin and J.R. Forrest, "Design Concepts for Active Phased-Array Modules," IEEE Proc., Part F; Communications, Radar and Signal Processing. Vol. 127, pp. 290-300:Aug. 1980.

3. A.A.A. DeSalles, "Optical Control of GaAs MESFET's," IEEE Trans. Microwave Theory Tech. Vol. MTT-31, pp. 812-820:Oct. 1983.
4. J.L. Gautier, D. Pasquet, and P. Pouvil, "Optical Effects on the Static and Dynamic Characteristics of a GaAs MESFET," IEEE Trans. Microwave Theory Tech. Vol. MTT-33, pp. 819-822:Sept. 1985.
5. H. Mizuno, "Microwave Characteristics of an Optically Controlled GaAs MESFET," IEEE Trans. Microwave Theory Tech. Vol. MTT-31, pp. 596-600:Jul. 1983.
6. B. Monemar, K.K. Shih, and G.D. Petit, "Some Optical Properties of the Al_xGal_{1-x}As Alloy System," J. Appl. Phys. Vol. 47, pp. 2604-2613:June 1976.
7. K.B. Bhasin, G.E. Ponchak, and T.J. Kascak, "Monolithic Optical Integrated Control Circuitry for GaAs MMIC-Based Phased Arrays," NASA TM-87183, 1985.
8. S.M. Sze, Physics of Semiconductor Devices, 2nd Ed., New York: Wiley-Interscience:1981.
9. G.J. Chaturvedi, R.K. Purohit, and B.L. Sharma, "Optical Effect on GaAs MESFETs," Infrared Phys. Vol. 23, pp. 65-68:1983.
10. M.T. Abuelma'atti, "Modeling DC Characteristics of HEMTs," Electron. Lett. Vol. 21, pp. 69-70:Jan. 1985.
11. K.L. Chopra, S. Major, and D.K. Pandya, "Transparent Conductors - A Status Review," Thin Solid Films, vol. 102, pp. 1-46:1983.
12. D.G. Parker, "Use of Transparent Indium Tin Oxide to Form a Highly Efficient 20 GHz Schottky Barrier Photodiode," Electron. Lett. Vol. 21, p. 778:Aug. 1985.
13. H.J. Sun, R.J. Gutmann, and J.M. Borrego, "Optical Tuning in GaAs MESFET Oscillators," 1981 IEEE MTT-S International Microwave Symposium Digest, J.E. Rave, Ed., New York: IEEE, pp. 40-42:1981.
14. F.J. Moncrief, "LEDs Replace Varactors for Tuning GaAs FETs," Microwaves, vol. 18, no. 1, pp. 12-13:Jan. 1979.
15. J.C. Gammel and J.M. Ballantyne, "An Integrated Photoconductive Detector and Waveguide Structure," Appl. Phys. Lett. Vol. 36, pp. 149-151, Jan. 1980.